Introduction to Nonlinear Control

Stability, control design, and estimation

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Introduction to Nonlinear Control: Stability, control design, and estimation

Part III: Observer Design and Estimation

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Introduction to Nonlinear Control

STABILITY, CONTROL DESIGN, AND ESTIMATION



So far:

- The concepts so far rely on the knowledge of the state $x \in \mathbb{R}^n$.
- The full state x is in general not known and only the output $y \in \mathbb{R}^p$ is available.
- \rightsquigarrow A controller design can not, in general, rely on the full state *x*.
- \rightsquigarrow An estimate \hat{x} of the state needs to be derived (observability, detectibility)
- If $\hat{x}(t) \rightarrow x(t)$ for $t \rightarrow \infty$, can \hat{x} be used for the definition of a feedback controller $u(\hat{x})$?

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Consider Linear systems:

$$\dot{x} = Ax + Bu, \qquad x(0) \in \mathbb{R}^n$$

 $y = Cx + Du$

- We assume that $y \in \mathbb{R}^p$ and $u \in \mathbb{R}^m$ are known, while the internal state $x \in \mathbb{R}^n$ and the initial condition x(0) are unknown.
- Assume that the matrix A is Hurwitz.



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• Introduce observer dynamics as a copy of the system

 $\dot{\hat{x}} = A\hat{x} + Bu, \qquad \hat{x}(0) \in \mathbb{R}^n$

- $\hat{x} \in \mathbb{R}^n$ estimate of the state $x \in \mathbb{R}^n$
- Estimation error $e = x \hat{x}$
- Error dynamics:

$$\begin{split} \dot{e} &= \dot{x} - \dot{\hat{x}} = Ax + Bu - A\hat{x} - Bu = A(x - \hat{x}) = Ae \\ \hat{x}(t) \rightarrow x(t) \quad \Leftrightarrow \quad e(t) \rightarrow 0 \quad \Leftrightarrow A \text{ Hurwitz} \end{split}$$



$$\dot{x} = Ax + Bu,$$
 $x(0) \in \mathbb{R}^n,$ (or $x^+ = Ax + Bu$)
 $y = Cx + Du$

Define observer dynamics:

$$\dot{\hat{x}} = A\hat{x} + Bu - L(y - \hat{y}),$$

$$\hat{y} = C\hat{x} + Du.$$

• output injection term $L \in \mathbb{R}^{n \times p}$



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 $\rightsquigarrow~$ The error dynamics are independent of u



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- $\rightsquigarrow~$ The error dynamics are independent of u
- A + LC has the same eigenvalues as $(A + LC)^T = A^T + C^T L^T$
- $\stackrel{\rightsquigarrow}{\to} \mbox{ If } (A,C) \mbox{ is observable, the poles of } A+LC \mbox{ can be} \mbox{ placed arbitrarily, i.e., } L \mbox{ can be defined such that } A+LC \mbox{ is Hurwitz.}$
- $\stackrel{\rightsquigarrow}{\to} \mbox{ If } (A,C) \mbox{ is detectable, then there exists } L \mbox{ such that } A+LC \mbox{ is Hurwitz.}$



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- → If (A, C) is observable, the poles of A + LC can be placed arbitrarily, i.e., L can be defined such that A + LC is Hurwitz.
- \leadsto If (A,C) is detectable, then there exists L such that A+LC is Hurwitz.
- See pole placement
- x can be approximated through \hat{x}



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- $x \text{ can be approximated through } \hat{x}$
- Controller design $u = K\hat{x}$?

Luenberger Observers & Controller design

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Controller design:

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Overall closed loop system

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ė	= [0	A + LC		e

- If (A, B) is controllable and (A, C) is observable, we can place the poles of the closed-loop system arbitrarily by choosing K and L.
- The convergence $|x(t)| \to 0$ and $|e(t)| \to 0$ for $t \to \infty$ can be guaranteed by designing L and K individually. \rightsquigarrow *separation principle*
- (The separation principle is only true for the asymptotic behavior)

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- (The separation principle is only true for the asymptotic behavior)

Alternative representation in terms of x and \hat{x} :

$$\left[\begin{array}{c} \dot{x} \\ \dot{\hat{x}} \end{array} \right] = \left[\begin{array}{c} A & BK \\ -LC & A+BK+LC \end{array} \right] \left[\begin{array}{c} x \\ \hat{x} \end{array} \right]$$

 \leadsto While the separation principle is not visible the dynamics capture the same information.

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- measurement noise: $w(\cdot): \mathbb{R} \to \mathbb{R}^p$ (depending on the sensors)

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The *minimum energy estimation* problem:

• For given $u(\cdot)$, $y(\cdot)$, find $\bar{x}: \mathbb{R}_{\leq t_0} \to \mathbb{R}^n$ for $t_0 \geq 0$, which satisfies the dynamics

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$$J_{\text{MEE}}(\bar{x}(t_0), v(\cdot)) = \int_{-\infty}^{t_0} (\tau)^T Q w(\tau) + v(\tau)^T R v(\tau) d\tau$$

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Note that:

• Design parameters: $Q \in S_{>0}^p$, $R \in S_{>0}^q$

• $J_{\text{MEE}}(\bar{x}(t_0), v(\cdot))$ is a function of $v(\cdot)$ but not $w(\cdot)$:

$$J_{\text{MEE}}(\bar{x}(t_0), v(\cdot)) = \int_{-\infty}^{t_0} v^T R v + (C\bar{x} + Du - y)^T Q (C\bar{x} + Du - y) d\tau$$

Given $u(\cdot), y(\cdot)$, find disturbance $v(\cdot)$ with minimum energy and an estimated state $\bar{x}(t_0)$ that explains the observed inputs and outputs.

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Given $u(\cdot)$, $y(\cdot)$, find disturbance $v(\cdot)$ with minimum energy and an estimated state $\bar{x}(t_0)$ that explains the observed inputs and outputs.

- Q large: penalize noise $w(\cdot)$; neglect disturbance
- R large: penalize disturbance $v(\cdot)$; neglect noise

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Theorem (The minimum energy estimator)

- Consider the perturbed linear system and assume that (A, \bar{B}) is controllable and (A, C) is detectable.
- Consider the optimization problem where the cost function is defined through positive definite matrices Q ∈ S^p_{≥0} and R ∈ S^q_{≥0}.
- Then there exists $S \in S_{>0}^n$ to the dual algebraic Riccati equation

 $AS + SA^T + \bar{B}R^{-1}\bar{B}^T - SC^TQCS = 0$

such that A - LC is Hurwitz, where $L = SC^TQ$.

• The minimum energy estimator is given by

 $\dot{\hat{x}} = A\hat{x} + Bu + L(y - C\hat{x} - Du)$

and the initial condition $\hat{x}(t_0) = \bar{x}_0$, $t_0 \in \mathbb{R}_{\geq 0}$.

Minimum Energy Estimator (and the Kalman Filter)

Remarks:

- The *minimum energy estimator* is derived using the *deterministic setting*
- In the stochastic setting the minimum energy estimator is related to the (cont. time) Kalman filter.
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• Assume $v(\cdot)$ and $w(\cdot)$ represent functions of zero-mean Gaussian white noise with covariance matrices satisfying

$$\begin{split} \mathbf{E}[v(t)v(\tau)^T] &= \delta(t-\tau)R^{-1},\\ \mathbf{E}[w(t)w(\tau)^T] &= \delta(t-\tau)Q^{-1},\\ \mathbf{E}[v(t)w(\tau)^T] &= 0 \end{split}$$

for all $t, \tau \in \mathbb{R}$ and Q > 0, R > 0.

Here:

- expected value: $E[\cdot]$:
- Dirac delta function: $\delta : \mathbb{R} \to \mathbb{R} \cup \{\infty\}$

$$\delta(t) = \left\{ \begin{array}{ll} \infty, & t=0\\ 0, & t\neq 0 \end{array} \right. \qquad \text{and} \qquad \int_{-\infty}^{\infty} \delta(t) dt = 1.$$

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Under these conditions

• \hat{x} obtained through the minimum energy estimator minimizes the expected value

$$\lim_{t \to \infty} \mathbf{E}\left[|x(t) - \hat{x}(t)|^2\right]$$

(which is used to derive the Kalman filter)

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Similarly, the minimum energy estimator and the Kalman filter can be derived in the discrete time setting.

Part I: Dynamical Systems

- 1. Nonlinear Systems -Fundamentals & Examples
- 2. Nonlinear Systems Stability Notions
- 3. Linear Systems and Linearization
- 4. Frequency Domain Analysis
- 5. Discrete Time Systems
- 6. Absolute Stability
- 7. Input-to-State Stability

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- 9. Control Lyapunov Functions
- 10. Sliding Mode Control
- 11. Adaptive Control
- 12. Introduction to Differential Geometric Methods
- 13. Output Regulation
- 14. Optimal Control
- 15. Model Predictive Control

Part III: Observer Design & Estimation

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- 17. Extended & Unscented Kalman Filter & Moving Horizon Estimation
- Observer Design for Nonlinear Systems